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Development, Verification, and Validation of a Parametric Cervical Spine Injury Prediction Model

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ABSTRACT

The objective of this investigation is to develop a high fidelity, parametric finite element model of the cervical spine motion segment using a hierarchical model verification and validation approach. A technique has been developed to accurately describe the geometry of the cervical spine using a set of unique geometry parameters that are easily measured from clinical imaging systems such as Computed Tomography (CT) scans and to efficiently convert this geometry into a well-defined finite element model. Cervical spine parameters were measured from CT scans collected from a total of 73 volunteers, 50 male and 23 female. The parametric finite element model development includes a hierarchical model verification and validation (V&V) procedure that consists of verifying the model performance at increasing levels of complexity. Currently there are four levels. The first level is the component level and includes the individual soft tissue material properties such as the cervical ligaments. The next level is a meso-component level consisting of the behavior of the intervertebral disc via an isolated vertebral body-disc-vertebral body structural construct. The third hierarchical level consists of a complete motion segment with all associated soft tissue components. The fourth level is the full cervical column. Each level in the hierarchy builds on the previous level ensuring a systematic model V&V process (i.e., providing evidence the right answer is obtained for the right reason). This investigation will result in four verified and validated computational models of the cervical spine: a small female (106 lb - 120 lb), a large female (136 lb - 150 lb), a small male (166 lb - 180 lb), and a large male (226 lb - 240 lb). These models will be able to predict injury under a variety of loading conditions and will have many applications in the fields of biomechanics and auto safety.

INTRODUCTION

Cervical spine numerical modeling has many uses in areas such as accident reconstruction, injury biomechanics, surgical analyses, and kinematic studies. Other applications of numerical modeling include the study of morphology and architecture of hard tissues, ligament and disc characteristics, spinal loading, and muscle morphometry and action (Harrison et al., 2004). Given the numerous applications of a cervical spine model, it is imperative to ensure that a numerical model has been verified and validated for its intended use; a model is only meant to represent the conditions in which it is validated (Ng et al., 2001).

Measured geometries of the cervical spine have been used to create numerous finite element models. In the model created by Ng et al. (2001), and also used by Teo et al. (2001), the geometry was created by digitally scanning a dried cervical spine specimen from a 68-year old man. Yang et al. (1998) created a model using cervical spine geometry obtained from magnetic resonance imaging (MRI) of a 50th percentile male. The widely used KTH model was constructed using vertebral geometries based on the CT images of a 27 year old male, that were then scaled to those of a 50th percentile male (Brolin et al., 2004). Although scaling techniques have been used to develop injury criteria for dummies of various sizes (Hilker et al., 2002), this may not be a viable approach. The cervical spine geometry of females is not simply a scaled down male geometry (Mordaka et al., 2003). Therefore, a parametric cervical spine model is needed to better represent the entire population that the model is going to represent. By employing a parametric finite element model approach, finite element models can be generated by simply inputting the new geometry parameter values saving time when numerous models are going to be created, and also allowing for probabilistic analyses.

Verification and validation studies form the crucial link between the development of the finite-element model and its ultimate intended use. They are the primary processes used in quantifying and building confidence in finite element models. Verification is the process of determining that a model implementation accurately represents the developer's conceptual description of the model and the solution to the model. Validation is the process of determining the degree to which a model is an accurate representation of the real world from the perspective of the intended uses of the model (American Institute of Aeronautics and Astronautics, 1998; Thacker, 2003). In short, verification deals with the mathematics associated with the model, whereas validation deals with the physics associated with the model (Roache, 1998). Hierarchical verification and validation starts from the smallest components of a finite element model increasing in complexity to the complete system model (Figure 1). The response of the model is validated at each level before continuing on to the next without modifying model parameters at the complete model level to fit the experimental data.

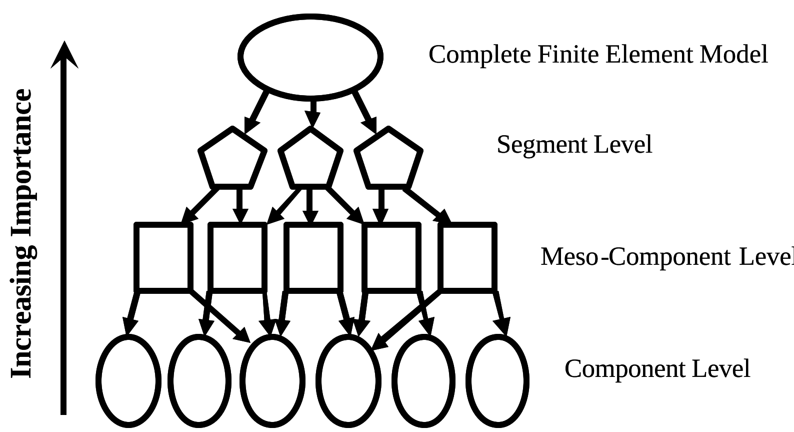

Figure 1: Verification and validation hierarchy.

The objective of this investigation is to develop a high fidelity, parametric finite element model of the cervical spine motion segment using a hierarchical model verification and validation approach. A technique will first be developed to accurately describe the geometry of the cervical spine using a set of unique geometry parameters that can be measured from Computed Tomography (CT) scans. The geometry will then be used to create a well-defined finite element model. Finally, the model will be verified and validated using a hierarchical approach.

METHODS

Parametric Model Development

A parametrically defined cervical vertebra was defined using a parametric solid modeling software package (Pro/ENGINEER) (Figure 2a). The finite element mesh was then created using TrueGrid from a surface representation of the solid model exported from Pro/Engineer (Figure 2b). The mesh was constructed in several partitions to ensure uniform fidelity and to more easily accommodate changes in the nominal motion segment geometry resulting from perturbations in geometry parameters. After the mesh was constructed, boundary conditions were assigned to the model, and a mesh refinement study was performed to determine the mesh that would be used for the probabilistic analysis.

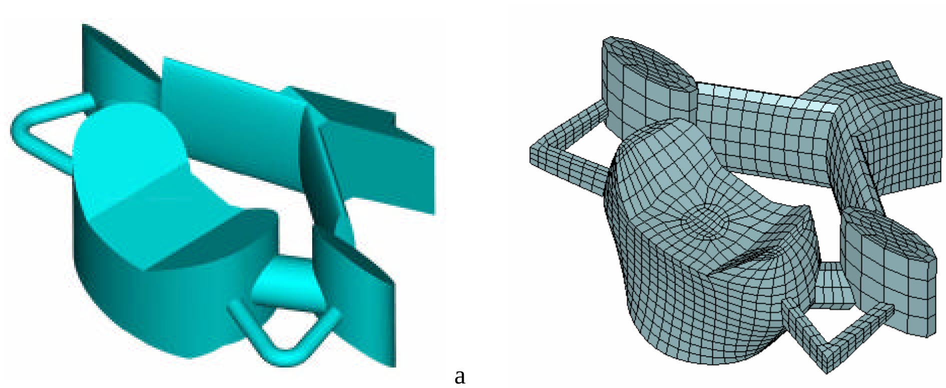
a b

Figure 2: Parametrically defined (a) solid model of the cervical vertebra and (b) mesh.

Geometry Parameter Measurement

CT scans of the cervical spine of 73 volunteers (23 female and 50 male) were obtained in digitized format. The CT image stacks were re-sliced to allow measurements on four different planes (Figure 3). A total of 35 parameters were measured for each vertebra, C3 through C7 (Figure 4). Four of the 35 parameters are angles, and were measured in degrees, whereas the remaining 31 parameters were measured in millimeters. A parameter index was included for each measurement: ap – articular process, pd – pedicle, sp – spinous process, tp – transverse process, and vb – vertebral body. All of the measurements were performed using a freely available image processing software package (ImageJ 1.34, National Institutes of Health, USA). A single researcher made all of the parameter measurements to maintain consistency and minimize error.

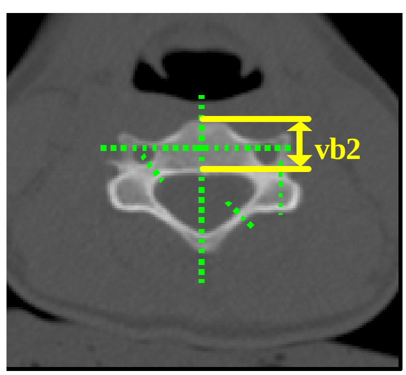

Figure 3: CT image slice of the cervical spine with dashed lines indicating the planes that re-slices were made on, and example of the vb2 measurement.

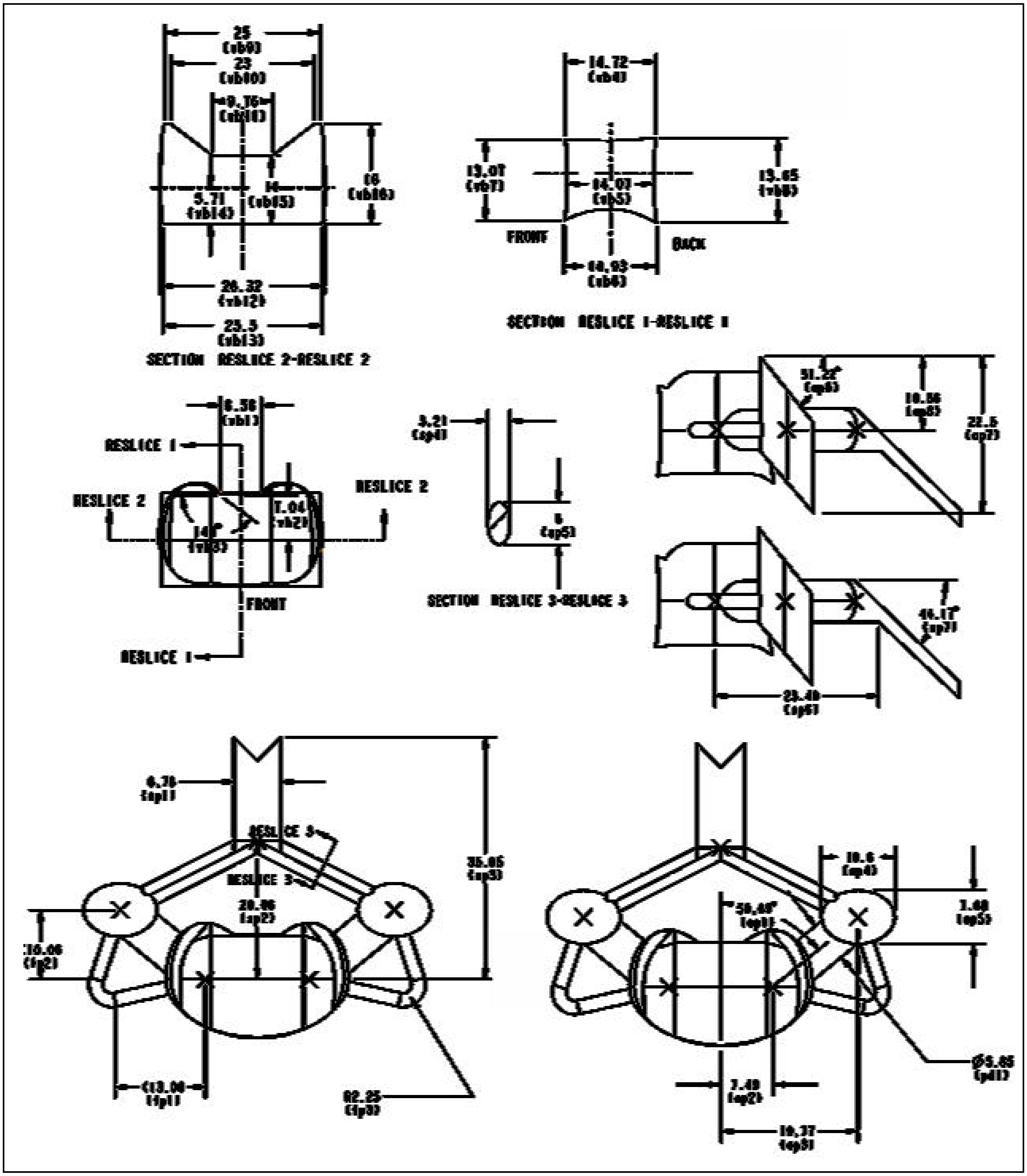

Figure 4: Diagram illustrating an example of the geometric parameters measured for each vertebra, C3 through C7 from the CT scans based upon the C5 vertebra solid model.

Verification and Validation Level 1: Component

The model was verified and validated by using the hierarchical verification and validation approach as described by Thacker (2003). The first level investigated was the component level, which included the individual cervical ligaments soft tissue material properties. Quasi-static and dynamic *in situ* axial tensile tests were conducted on the anterior longitudinal ligament (ALL), the posterior longitudinal ligament (PLL), interspinous ligaments (ISL), joint capsule (JC) and ligamentum flavum (LF) (Yoganandan et al., 2000). The results of these postmortem human subject (PMHS) specimen tests were used to define the geometry and material model parameters for each ligament. A transversely isotropic hyperelastic material model with viscoelasticity (LS-DYNA, LSTC, Livermore CA) was used in modeling the ligaments. Using an optimization routine, the ligament finite element material model parameters were fit to the test data. The finite element model of each of the ligaments (ALL, PLL, ISL, JC, LF) was then tested in the same conditions as the PMHS specimen tests were conducted and comparisons were made between their responses. Any changes that needed to be made to the finite element models of the ligaments were made at this level.

Verification and Validation Level 2: Meso-Component

The next level was a meso-component level consisting of the behavior of the intervertebral disc, tested in tension and compression via an isolated vertebral body-disc-vertebral body structural construct. The finite element model of the disk consists of a viscoelastic annulus and a fluid nucleus. Again, laboratory tests were conducted and comparisons were made between the finite element model response and those of the PMHS specimens. Any changes that needed to be made to the intervertebral disc finite element model were made at this level.

Verification and Validation Level 3: Motion Segment

The third hierarchical level consisted of a complete motion segment with all associated soft tissue components. At this level, each motion segment set (C3-C4, C4-C5, C5-C6, C6-C7) was tested in pure moment conditions using PMHS specimens (Wheeldon et al., 2006). The segments were loaded with a 2 Nm moment in flexion, extension, axial rotation, and lateral bending and the resulting rotations recorded. Comparisons were made to the finite element models loaded under equivalent conditions. At this level no changes were made to the finite element model to alter its response.

Verification and Validation Level 4: Full Cervical Spine

The fourth and most complex level was the full cervical spine column tested in flexion, extension, axial rotation, and lateral bending. The C3 through T1 motion segment of PMHS specimens was constrained at T1 while it was loaded with a 2 Nm moment at C3 (Wheeldon et al, 2006). At this level, the finite element models of the vertebral bodies, intervertebral discs, and their corresponding soft tissues were assembled. No changes were made to the finite element model components when comparisons were made with the full cervical spine.

RESULTS

Once all of the parameters were measured from the volunteer CT scans, they were entered into a database. The values for the 35 parameters at each vertebral level were averaged into four different groups: small female (106 lb - 120 lb), large female (136 lb - 150 lb), small male (166 lb - 180 lb), and large male (226 lb - 240 lb). The resulting average parameters were input into the parametric finite element model resulting in the creation of four different finite element models (Figure 5).

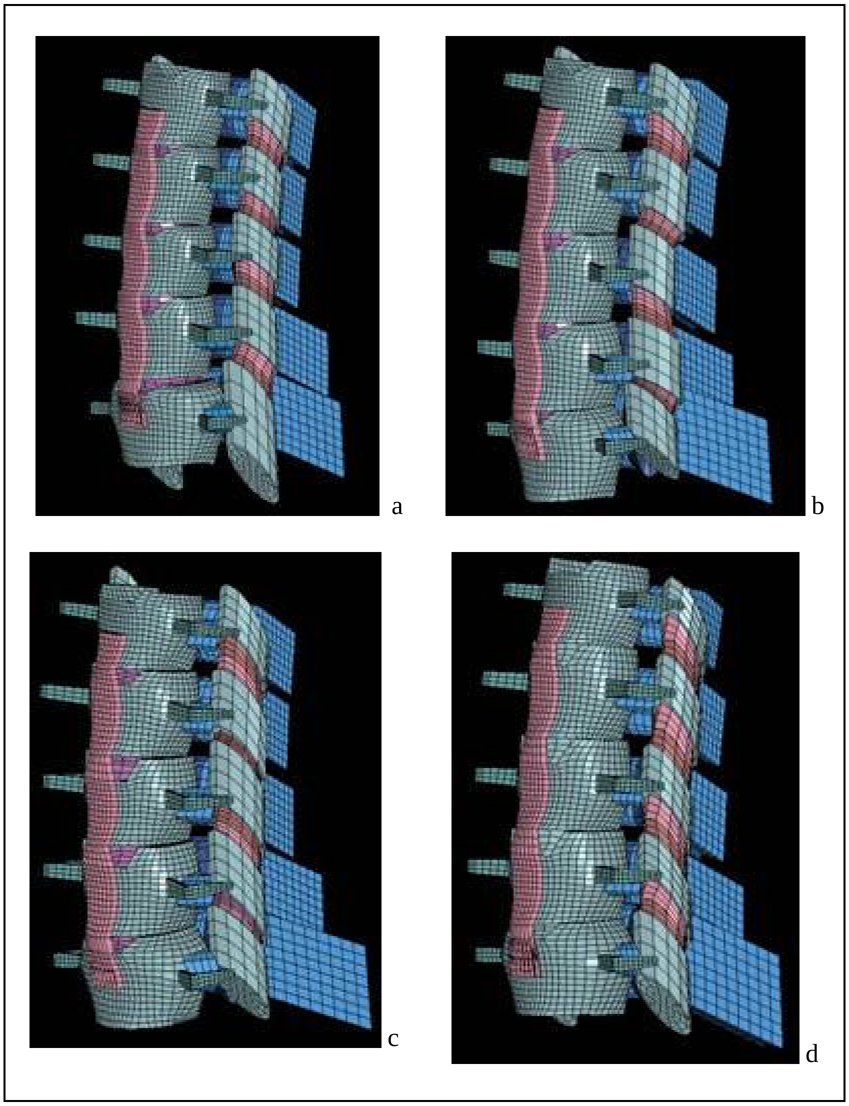

Figure 5: Finite element models created using the average geometry parameters for each weight group: (a) small female (106 - 120 lbs), (b) large female (136 - 150 lbs), (c) small male (166 - 180 lbs), and (d) large male (226 - 240 lbs).

Verification and Validation Level 1: Component

The ligament finite element models compared well to both the quasi-static and dynamic experimental data (Figures 6 - 7). The ligaments presented in this report are not weight or gender specific, and so these material models were used in both weight groups of the male and female models. The static tests show that the ligaments have a non-linear component. Figure 6 shows that the soft tissue material model captures this behavior well. Dynamic relaxation tests were performed at 25% strain. The six term Prony series viscoelastic parameters were perturbed until the model's response fit the test data. Figure 7 shows that the model response fits the test results quite well.

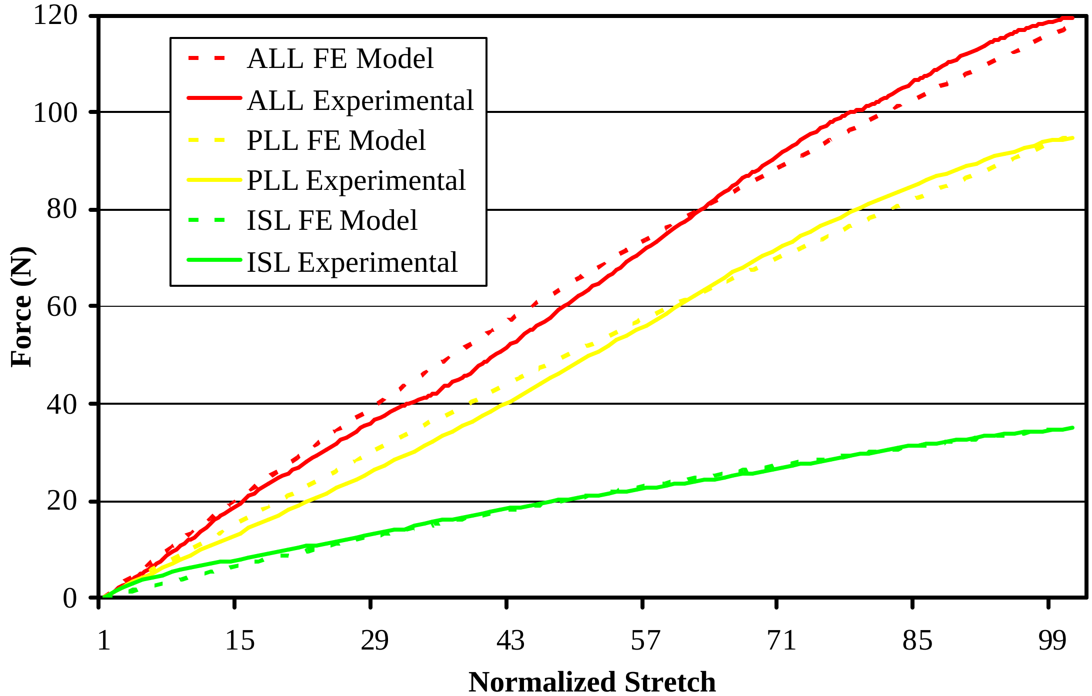

Figure 6: Ligament finite element (FE) models compared to the quasi-static experimental data for the ALL, PLL, and ISL.

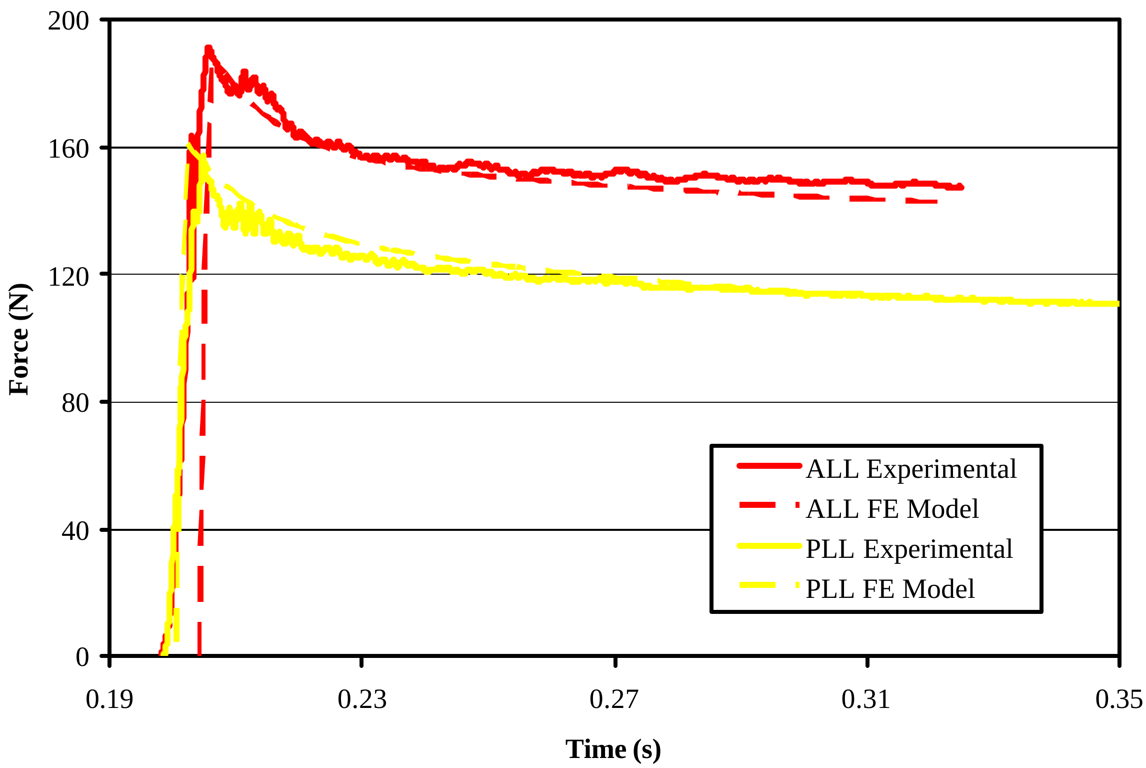

Figure 7: Ligament finite element (FE) models compared to the dynamic experimental data for the ALL and PLL.

Verification and Validation Level 2: Meso-Component

The force versus displacement responses of the intervertebral discs varied between the male and female specimens tested in compression and tension. Due to the small number of specimens, only one intervertebral disc finite element model was created based upon the experimental results. The parameters of the material model were tuned to best fit both the compression and tension data of both the male and female specimens; this included the bulk modulus and viscoelastic parameters. The hysteresis response of the intervertabral disc PMHS specimens in tension and compression was well captured by the finite element model when it was tested in the same manner (Figures 8-9).

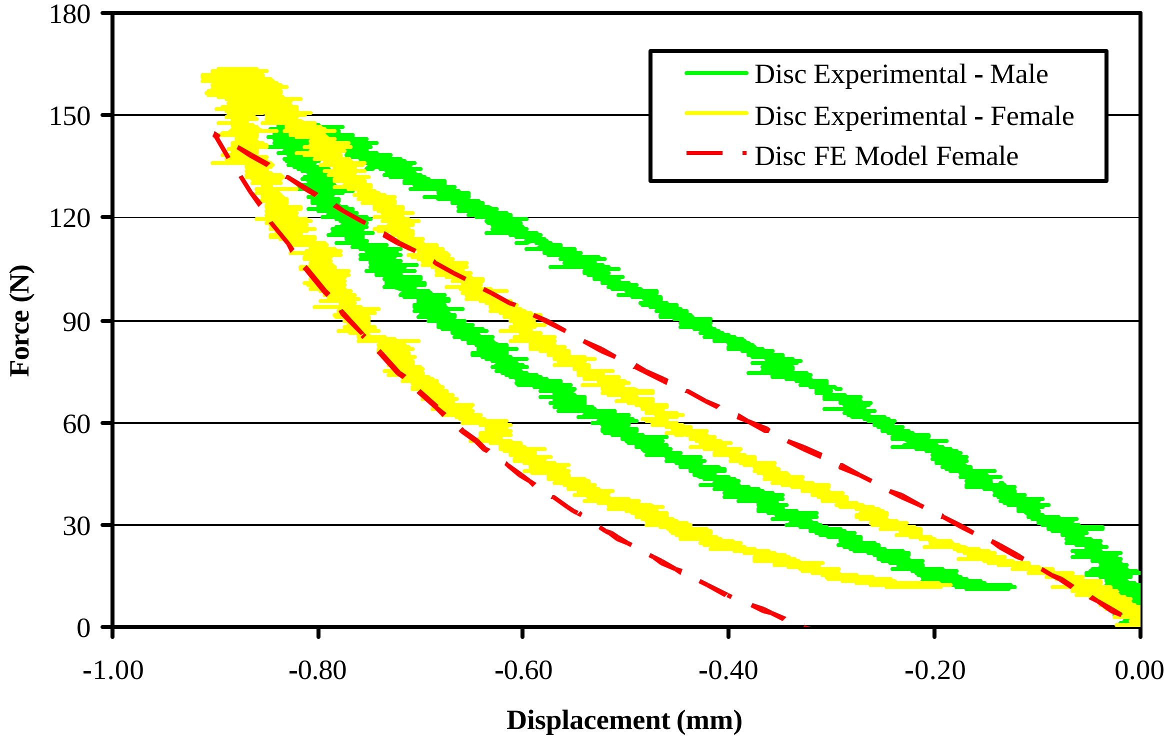

Figure 8: Disc finite element (FE) model compared to the experimental data for the disc in compression between two vertebral bodies.

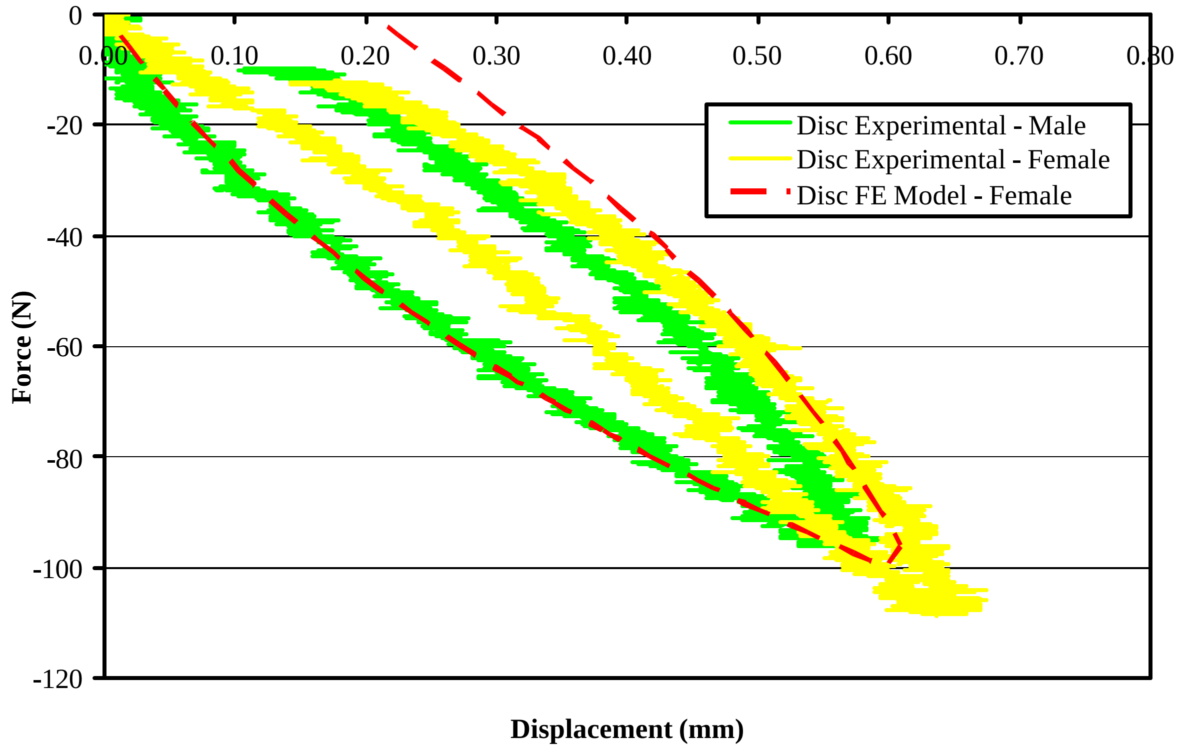

Figure 9: Disc finite element (FE) model compared to the experimental data for the disc in tension between two vertebral bodies.

Verification and Validation Level 3: Motion Segment

Each of the finite element motion segments compared fairly well to the experimental data for all four of the weight groups in flexion, extension, axial rotation, and lateral bending. Several of these comparisons are described here (Figures 10-13). In the following figures, the solid green lines show the average response of the PMHS experiments bounded by plus and minus one standard deviation. The dashed red, yellow, light blue, and dark blue lines represent the small female, large female, small male, and large male finite element model responses, respectively.

In the flexion and extension rotational responses of the motion segments, a "slack" effect can be seen (Figures 10-11). The initial portions of the responses have a large slope until approximately 0.5 Nm, where the ligaments are not playing as large of a role. Once the ligaments have been stretched to a certain point, they influence the rotational response rather than the vertebral geometry or other factors.

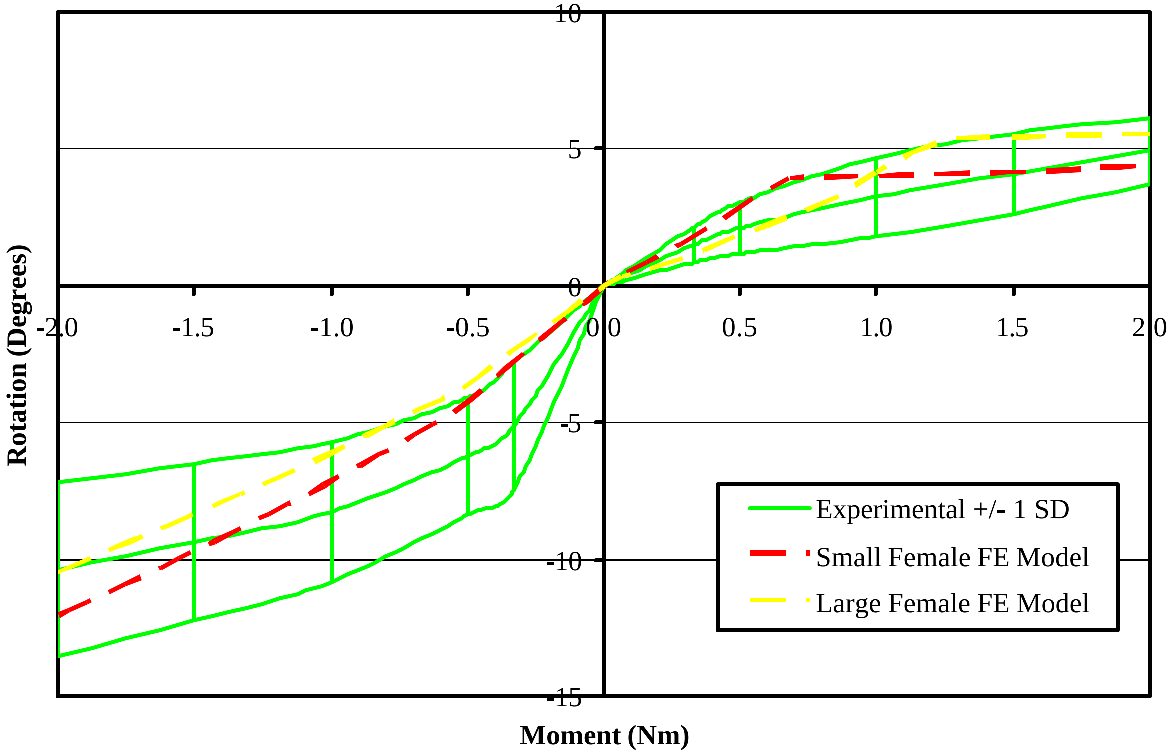

Figure 10: Finite element (FE) models compared to the experimental data for the C4-C5 motion segment rotational response in flexion and extension.

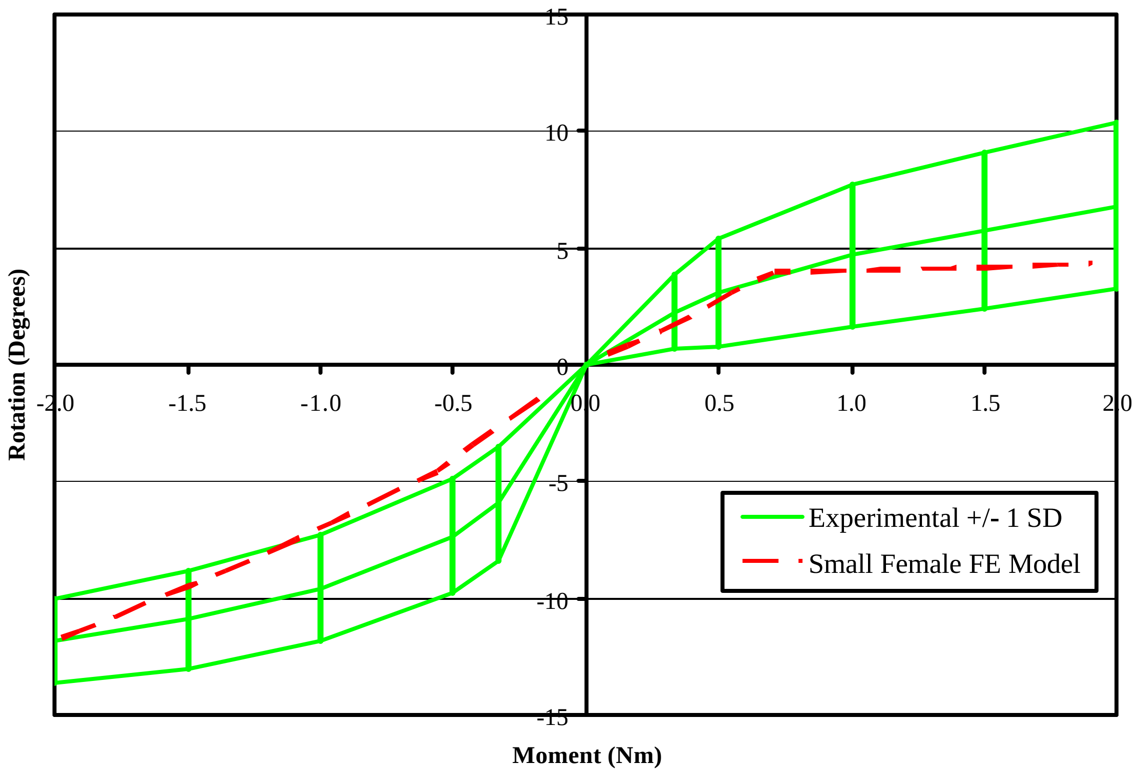

Figure 11: Finite element (FE) models compared to the experimental data for the C5-C6 motion segment rotational response in flexion and extension.

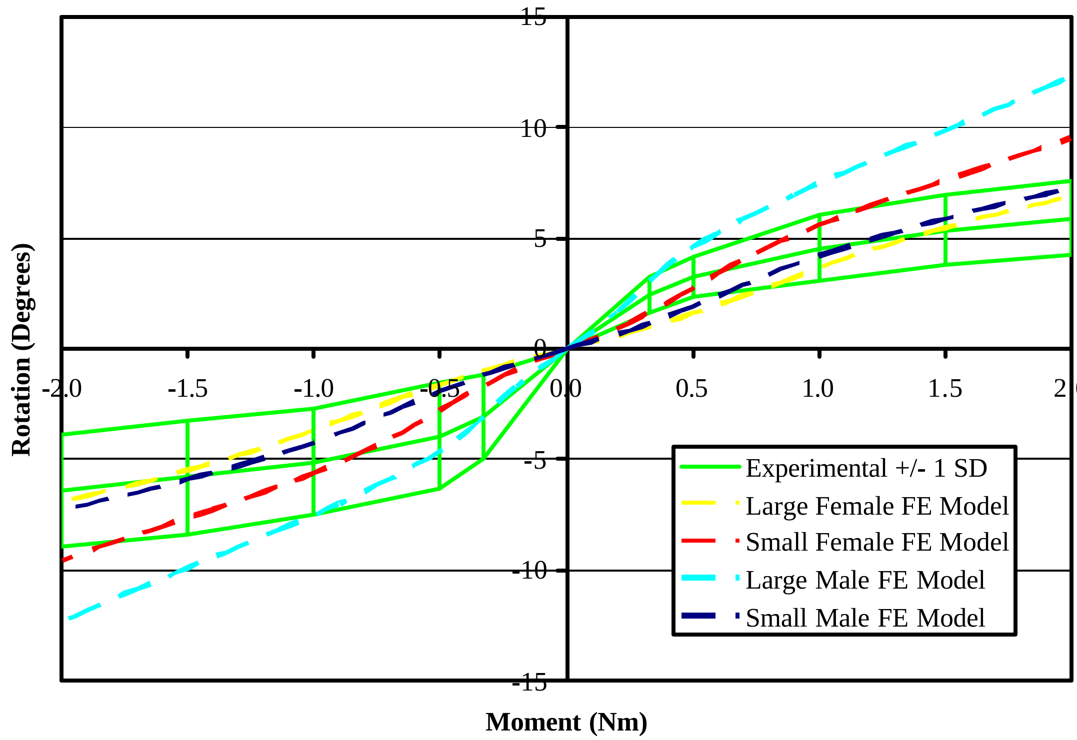

Figure 12: Finite element (FE) models compared to the experimental data for the C5-C6 motion segment rotational response in lateral bending.

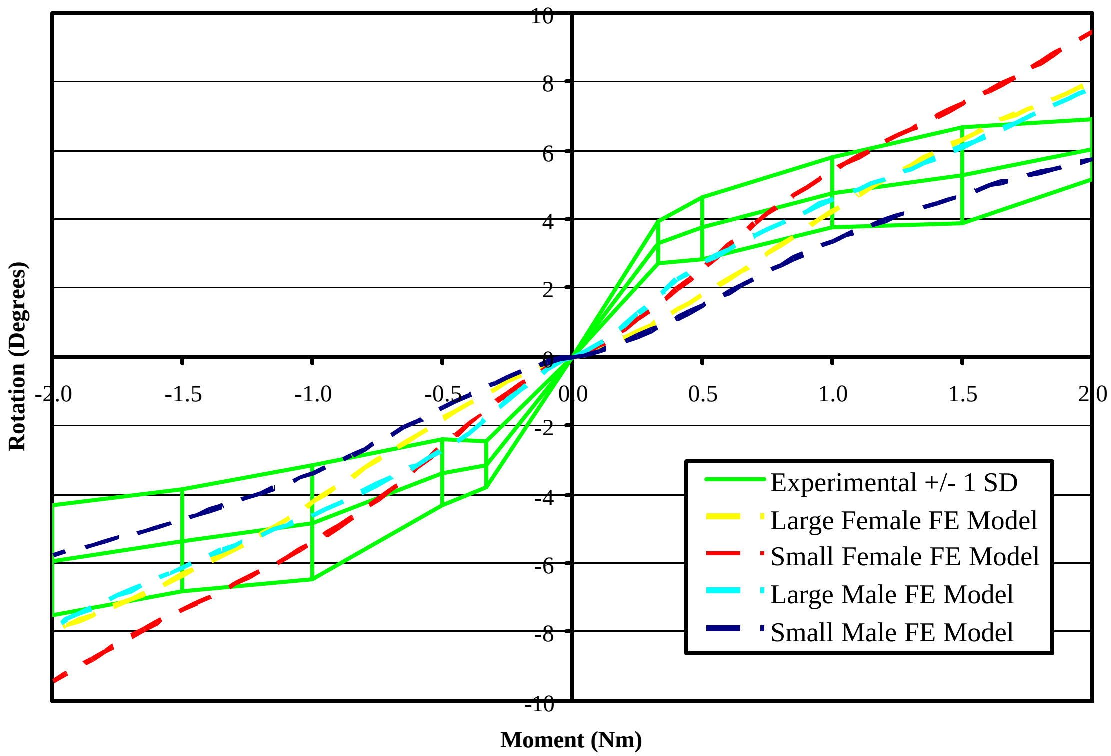

Figure 13: Finite element (FE) models compared to the experimental data for the C5-C6 motion segment rotational response in axial rotation.

Verification and Validation Level 4: Full Cervical Spine

The full cervical spine column, from C3 to T1, will be tested in flexion, extension, axial rotation, and lateral bending. The initial results from this stage include the flexion and extension responses of the small female finite element model (Figure 14). The rotation-moment endpoints of both the flexion and extension responses of the small female finite element model fall on the average value of the PMHS responses. The entire response in extension in fact falls on the average of the PMHS responses. It is imperative to reiterate that the finite element model was built using the hierarchical verification and validation bottom up approach to achieve these results. The correct answers are being achieved for the right reasons.

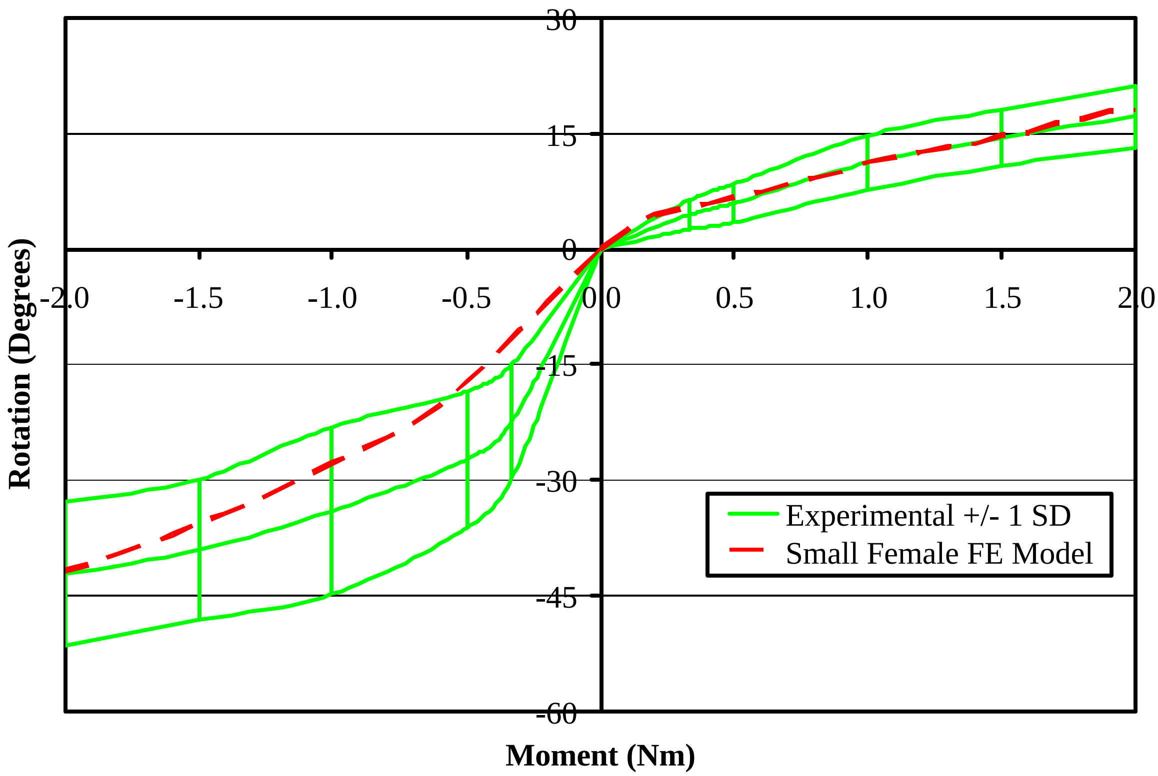

Figure 14: Small female finite element (FE) model compared to the experimental data for the full cervical spine (C3-T1) rotational response in flexion and extension.

DISCUSSION

Because the cervical spine model presented here is parametric, it offers distinct possibilities not offered by other cervical spine models. A personalized finite element model can be created for any individual who has a CT scanned performed. In a matter of hours, measurements can be taken from a patient's CT scan and input into the parametric finite element model. There are numerous applications for a model of this type. Additional weight groups can also be considered and the response of different spinal geometries can be investigated. This model is being used in probabilistic analyses, which will yield injury probability distributions and confidence levels. The model is currently used for military applications but can also be used in accident reconstruction and clinical applications.

The research and results presented here are a work in progress. Additional verification and validation will complete the four finite element cervical spine models. Injury thresholds and criteria will need to be incorporated into the model to make it a valuable injury prediction model. The near future plans for the model are to add the head through C2 vertebral geometries and their corresponding soft tissue and musculature. The effects of active muscles will also be evaluated. Ultimately, the model will be extended to include the full spinal column.

CONCLUSIONS

Four high fidelity parametric finite element models of the cervical spine have been created using a hierarchical model verification and validation approach: a small female (106 lb - 120 lb), a large female (136 lb - 150 lb), a small male (166 lb - 180 lb), and a large male (226 lb - 240 lb). A technique has also been developed to accurately describe the geometry of the cervical spine using a set of 175 unique geometry parameters that can easily be measured from CT images. These FE models will be able to predict injury under a variety of loading conditions and will have many applications in the fields of biomechanics and automotive safety.

ACKNOWLEDGEMENTS

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DISCUSSION

PAPER: **Development, Verification and Validation of a Parametric Cervical Spine Injury Prediction Model**

PRESENTER: ***Amber R. Bonivtch, Southwest Research Institute, Medical College of Wisconsin, GADAB Engineering***

QUESTION: *Guy Nusholtz, Daimler Chrysler*
You have a fairly extensive validation. How did you do your verification? You mentioned two things: verification and validation, and you just talked about validation.

ANSWER: *Dan McMillan, Southwest Research Institute*
I can answer that question. We consider verification our Level 1 verification where we're choosing the correct equations and model the nonlinear behavior…but we're choosing…

A: To answer the question, we consider verification choosing the correct mathematical model to predict the behavior, the nonlinear behavior of the ligaments at Level 1. So in this case, we're using a quasi-linear viscoelastic model. So, validation in our minds is running the simulation and comparing it to an experiment, experimental results without any model tweaking. Verification is choosing the correct equation, determining the correct parameters for those equations and making sure that the behavior of that mathematical model matches the experiment.

Q: So in this case, when you just take a ligament and you separate it, comparing the response of that ligament to the response of the model, that's verification of the numerical procedures.

A: Right.

Q: Okay. And that's how you're interpreting that, correct? Okay. Thank you.

One other question: You're validating—You're gonna use this for injury, but you don't seem to have any validation of a damage model on the side of your thing. So, how is that going to--?

A: Yeah. We'll get there. Right now, we're just wanting to make sure it responds in the same manner as a human does.

Q: Okay. So, this is just non-injurious type of response.

A: Right. This is just the—We haven't looked at the injuries at all. It's not right there yet. It'll get there after we, as the musculature and everything else make it more biofidelic before we start looking at injuries. Doing a comparison now really wouldn't help anything.

Q: Okay. Thank you.

Q: *Erik Takhounts, NHTSA*
I promised to have a question for you, so here it is. Having been in the modeling business for, like, I don't know, 15 or 20 years, I never in my entire life, through all my modeling ever achieved what you are trying to achieve. I have found myself, all of the time, going back, changing the parameters, what you call tweaking [chuckles] and going through the whole cycle again and again and again until I get some kind of optimal solution where it doesn't fit all the curves perfectly but sort of does the job what it's intended to do, which is simulate crash situation or something.

A: *Amber R. Bonivtch, Southwest Research Institute*
Right.

Q: I just wanted to kind of warn you from being overwhelmed in this thing in terms of your validation or verification—the end being method because to me it sounds a little bit too optimistic at this point.

A: And it does take a long time to—that's one thing you pointed out: It takes a long time to do this, but we've been given an opportunity to, so it's available to us right now to be able to do that.

Q: The other question is: The model is not a physical system. The model is a mathematical representation of the physical system and especially this simplified model, which is finite element model, it has a huge junk attached to every simulation. That's what I call numerical junk that you—After every simulation, you have to go and isolate what is in your response actually junk and what is your physical response of the actual system. And I found that without adding this numerical junk to the whole simulation process, you are basically searching in waters that's solutions have never been in. Alright? So, just another, I think, a comment or you can answer that if you can: How are you going to include this numerical junk hourglass so they are just a stability, just what the software manufacturer does to make a model run? How are you going to include all those parameters into your V& V process?

A: That's something to think about. We haven't—That hasn't been brought to our attention.

Q: Alright. Thank you.

Q: *Randy Ching, University of Washington*
Just a quick question: Excellent and ambitious study and I just want to follow-up on Erik's topic about the validation and verification. We're running models and I'm sure a lot of other people in this audience are also trying to validate their models. And, I guess the question I have is at what point would you consider your model validated?

A: Right.

Q: Are you trying to fit all of your response curves, your moment angle curves within one standard deviation? And if you've got some that don't fit it, does that mean that your model is not valid?

A: *Dan McMillan, Southwest Research Institute*
That's a good point. I'll take this question. As you'll see in our next talk, we're also doing a probabilistic analysis and part of our overall V&V procedure is comparing experimental results to numerical results in a probabilistic setting. So, we'll have a statistical set of experiments and we'll also have a simulated statistical set of simulations, and we'll do specific statistical tests like you would test for differences and that's how we'll determine if the model is valid using a statistical test.

Q: You'll present that in the next—

A: Well, we're not there. We'll show you the methodology that we're using.

Q: Is that an apt test or--?

A: We could use an apt test, but what I've done in the past is compare distributions of responses using a KS test or some other nonparametric test to test the differences between probability distributions.

Q: Love your topic.